

one obtains

$$P_m/P_x = [\rho_m^0 D_m / \rho_x^0 D_x] \times [(\rho_x^0 D_x + \rho_r^0 D_r) / (\rho_m^0 D_m + \rho_r^0 D_r)]. \quad (2)$$

If one makes the acoustic approximation $\rho_r^0 D_r = \rho_x^0 D_x$, Eq. (2) simplifies to

$$P_x = (P_m / 2\rho_m^0 D_m) (\rho_x^0 D_x + \rho_m^0 D_m). \quad (3)$$

Error analysis shows P_x to be quite insensitive to error in $\rho_r^0 D_r$; for example, in Composition B a 10% error in $\rho_r^0 D_r$ corresponds only to a 1% error in P_x . A more precise treatment of the interface interaction by W. Fickett and R. D. Cowan⁷ gives for the cases of interest in this paper values of explosive pressure only about 1% higher than those resulting from the acoustic approximation.

If in Eq. (3) one identifies P_m as P_m^* and P_x as the C-J pressure (P_{cj}) of the explosive, then P_{cj} can be established since ρ_x^0 and ρ_m^0 are the simply measurable initial densities of the explosive and the inert, D_x is the

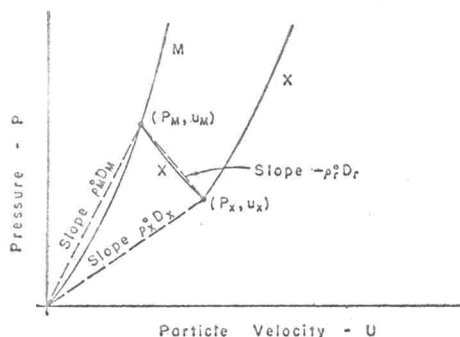


FIG. 3. Interaction at the interface between explosive and inert material in contact with it. *M* is the inert material Hugoniot; the *X*'s are Hugoniot for the reacted products of the explosive.

readily measurable detonation velocity⁸ and D_m^* and P_m^* are available from equation of state data if one hydrodynamic variable of this state is measured.⁹ The quantity established in these experiments was the free-surface velocity (U_{fs}^*).

An alternative method of establishing the C-J state, which minimizes the hitherto neglected effect of the reflected wave in the explosive on the reaction kinetics, is to establish the P_m^* state for each of several inert materials of different shock impedance. The state points define a curve in the pressure-particle velocity plane which closely approximates the locus of all possible shocked and rarefied states (for one direction of wave travel) from the C-J state of the explosive. It differs from this locus only insofar as the wave reflected back into the explosive affects the reaction kinetics; however, the amplitude of the reflected wave approaches zero as

⁷ R. D. Cowan and W. Fickett, *J. Chem. Phys.* 24, 932 (1956).

⁸ Campbell, Malin, Boyd, and Hull, *Rev. Sci. Instr.* 27, 567 (1956).

⁹ Walsh, Rice, McQueen, and Yarger, *Phys. Rev.* (to be published).

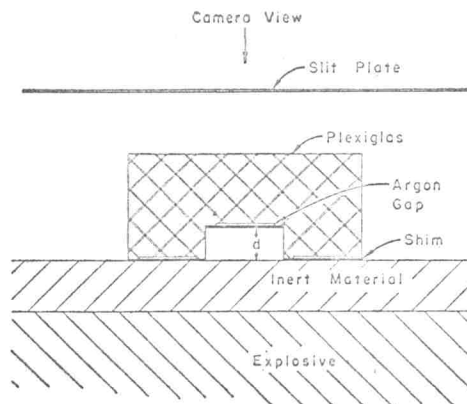


FIG. 4. Plexiglas block assembly for measurement of free-surface velocity of an explosive-driven plate.

one approaches the C-J state on this curve. The C-J state must also lie on the line $P_{cj}/U_{cj} = \rho_x^0 D_x$ (where U_{cj} is the C-J particle velocity). The C-J point is thus established as the intersection of this line with the aforementioned curve at the point where the perturbation of the reaction by a reflected wave is minimized.

EXPERIMENTAL TECHNIQUE

The value of free-surface velocity corresponding to P_m^* for a given explosive and inert material was determined by measurement of free-surface velocity of an explosive-driven plate as a function of plate thickness. These velocities were measured photographically by use of a rotating-mirror smear camera with a writing speed of 3.2 mm/ μ sec. A Plexiglas block assembly such as that of Figs. 4 and 5 was placed on the surface to be studied. This was viewed by the camera through a slit and swept on the film in a direction perpendicular to the slit image. When the explosive-driven plate on which such an assembly is placed begins to move, the argon gaps near the plate surface are closed first and yield a brilliant

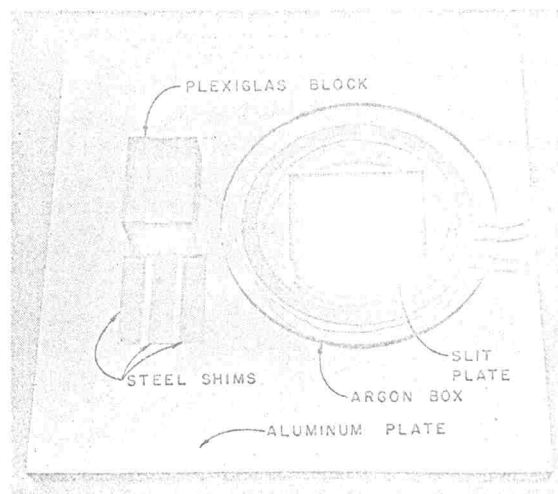


FIG. 5. Disassembled parts of the plate assembly for a free-surface velocity record such as shown in Fig. 6.